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Computer Implementation of the DRBEM for Studying the Generalized Thermo Elastic Responses of Functionally Graded Anisotropic Rotating Plates with Two Relaxation Times

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Abstract

A numerical computer model based on the dual reciprocity boundary element method (DRBEM) is extended to study the generalized thermo elastic responses of functionally graded anisotropic rotating plates. In the case of plane deformation, a predictor-corrector implicit-explicit time integration algorithm was developed and implemented for use with the DRBEM to obtain the solution for the displacement and temperature fields in the context of the Green and Lindsay theory. Numerical results that demonstrate the validity of the proposed method are also presented in the tables.

Keywords: Thermo elasticity; rotation; functionally graded material; anisotropic; dual reciprocity boundary element method.

1 Introduction

In recent years, the dynamical problem of thermo elasticity for an anisotropic material becomes more important due to its many applications in modern aeronautics, astronautics, earthquake engineering, soil dynamics, mining engineering, plasma physics, nuclear reactors and high-energy particle accelerators for instance. Biot [1] introduced the classical coupled thermo-elasticity theory (CCTE) to overcome the first shortcoming in the classical thermo-elasticity theory (CTE) introduced by Duhamel [2] and Neuman [3] where it predicts two phenomena not compatible with physical observations. First, the equation of heat conduction of this theory does not contain any elastic terms. Second, the heat equation is of a parabolic type, predicting infinite speeds of propagation for heat waves. Most of the approaches that came out to overcome the unacceptable

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prediction of the classical theory are based on the general notion of relaxing the heat flux in the classical Fourier heat conduction equation, thereby introducing a non-Fourier effect. One of the simplest forms of this equation is due to the work of Lord and Shulman [4] who introduced extended thermo-elasticity theory (ETE) with one relaxation time by constructing a new law of heat conduction to replace the classical Fourier's law. This law contains the heat flux vector as well as its time derivative. It contains also new constant that acts as relaxation time. Since the heat equation of this theory is of the wave-type, it automatically ensures finite speeds of propagation for heat and elastic waves. Green and Lindsay [5] included a temperature rate among the constitutive variables to develop a temperature-rate-dependent thermo-elasticity theory (TRDTE) that does not violate the classical Fourier's law of heat conduction when the body under consideration has a center of symmetry; this theory also predicts a finite speed of heat propagation and is known as the theory of thermo elasticity with two relaxation times. According to these theories, heat propagation should be viewed as a wave phenomenon rather than diffusion one. Relevant theoretical developments on the subject were made by Green and Naghdi [6,7] they developed three models for generalized thermo elasticity of homogeneous isotropic materials which are labeled as model I, II and III. The nature of these theories are such that when the respective theories are linearized, model I in Green and Naghdi [7] corresponds to the CTE theory based on Fourier's law, whereas the linearized versions of model II and III theories are of different nature. The entropy flux vector in model II and III (i.e. Thermo-elasticity without energy dissipation (TEWOED) and Thermo-elasticity with energy dissipation (TEWED)) models are determined in terms of potential that also determines stress. It is hard to find the analytical solution of a problem in a general case, therefore an important number of engineering and mathematical papers devoted to the numerical solution have studied the overall behavior of such materials [8-27].

Functionally graded materials (FGMs) are made of a mixture with arbitrary composition of two different materials, and the volume fraction of each material changes continuously and gradually. The FGMs concept is applicable to many industrial fields such as aerospace, nuclear energy, chemical plant, electronics, biomaterials and so on. Works by Skouras et al. [28], Mojdehi et al. [29], Loghman et al. [30] and Mirzaei and Dehghan [31] are examples involving functionally graded materials.

One of the most frequently used techniques for converting the domain integral into a boundary one is the so-called dual reciprocity boundary element method (DRBEM). This method was initially developed by Nardini and Brebbia [32] in the context of two-dimensional (2D) elasto dynamics and has been extended to deal with a variety of problems wherein the domain integral may account for linear-nonlinear static-dynamic effects. A more extensive historical review and applications of dual reciprocity boundary element method may be found in Brebbia et al. [33], Wrobel and Brebbia [34], Partridge and Brebbia [35], Partridge and Wrobel [36] and Fahmy [37-40].

The main objective of this paper is to study the generalized thermo elasticity problems in a rotating anisotropic functionally graded plate in the context of the Green and Lindsay theory. A predictor-corrector implicit-explicit time integration algorithm was developed and implemented for use with the dual reciprocity boundary element method (DRBEM) to obtain the solution for the temperature and displacement fields. The accuracy of the proposed method was examined and confirmed by comparing the obtained results with those known before.

2. Formulation of the Problem

Consider a Cartesian coordinates system Oxyz as shown in Fig. 1. We shall consider a functionally graded anisotropic plate rotating about it with a constant angular velocity. The plate occupies the region R={(x,y,z):0<x<_γ,0<y<_β,0<z<_α} with graded material properties in the thickness direction.

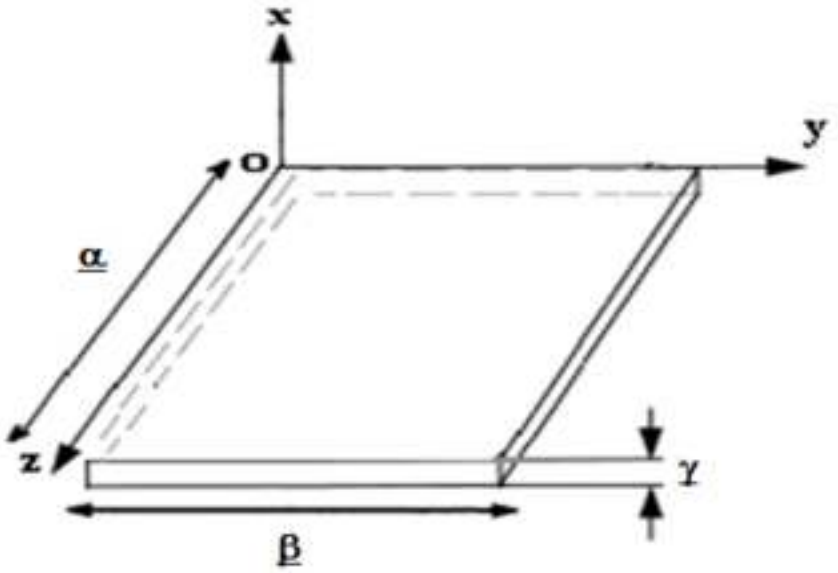

Fig. 1. The coordinate system of the plate

In this paper, the material is functionally graded along the 0x direction. Thus, the governing equations of generalized thermo-elasticity in the context of the Green and Lindsay theory can be written in the following form:

$$\sigma_{ab,b} - \rho(x+1)^m \omega^2 x_a = \rho(x+1)^m \ddot{u}_a, \tag{1}$$

$$\sigma_{ab} = (x+1)^m \left[C_{abfg} u_{f,g} - \beta_{ab}(T - T_0 + \tau_1 \dot{T})\right], \tag{2}$$

$$k_{ab} T_{,ab} = \beta_{ab} T_0 \dot{u}_{a,b} + \rho c (x+1)^m \left[\dot{T} + \tau_2 \ddot{T}\right]. \tag{3}$$

where σ_{ab} is the mechanical stress tensor, u_k is the displacement, T is the temperature, C_{abfg} and β_{ab} are respectively, the constant elastic moduli and stress-temperature coefficients of the anisotropic medium, ω is the uniform angular velocity, k_{ab} are the thermal conductivity coefficients satisfying the symmetry relation $k_{ab} = k_{ba}$ and the strict inequality $(k_{12})^2 - k_{11}k_{22} < 0$ holds at all points in the medium, ρ is the density, c is the specific heat capacity, τ is the time, τ_1 and τ_2 are mechanical relaxation times.

3. Numerical Implementation

Making use of (2), we can write (1) as follows

$$L_{gb}u_f = \rho\ddot{u}_a - \left(D_a T + \Lambda D_{a1f}u_f - \rho\omega^2 x_a\right) = f_{gb}, \tag{4}$$

where

$$L_{gb} = D_{abf}\frac{\partial}{\partial x_b}, D_{abf} = C_{abfg}\varepsilon, \varepsilon = \frac{\partial}{\partial x_g}, \Lambda = \frac{m}{x+1},$$

$$D_a = -\beta_{ab}\left(\frac{\partial}{\partial x_b} + \delta_{b1}\Lambda + \tau_1\left(\frac{\partial}{\partial x_b} + \Lambda\right)\frac{\partial}{\partial \tau}\right), f_{gb} = \rho\ddot{u}_a - \left(D_a T + \Lambda D_{a1f}u_f - \rho\omega^2 x_a\right).$$

The field equations can now be written in operator form as follows

$$L_{gb}u_f = f_{gb}, \tag{5}$$

$$L_{ab}T = f_{ab}, \tag{6}$$

where the operators L_{gb} and f_{gb} are defined in equation (4), and the operators L_{ab} and f_{ab} are defined as follows

$$L_{ab} = k_{ab}\frac{\partial}{\partial x_a}\frac{\partial}{\partial x_b}, \tag{7}$$

$$f_{ab} = \rho c(x+1)^m\left[\dot{T} + \tau_2\ddot{T}\right] + \beta_{ab}T_0\dot{u}_{a,b}. \tag{8}$$

Using the weighted residual method (WRM), the differential equation (5) is transformed into an integral equation

$$\int_R (L_{gb}u_f - f_{gb})u^*_{da}\, dR = 0. \tag{9}$$

Now, we choose the fundamental solution u^*_{df} as weighting function as follows

$$L_{gb}u^*_{df} = -\delta_{ad}\delta(x,\xi). \tag{10}$$

The corresponding traction field can be written as

$$t^*_{da} = C_{abfg}u^*_{df,g}n_b. \tag{11}$$

The thermo elastic traction vector can be written as follows

$$t_a = \frac{\bar{t}_a}{(x+1)^m} = \left(C_{abfg}u_{f,g} - \beta_{ab}(T - T_0 + \tau_1\dot{T})\right)n_b. \tag{12}$$

Applying integration by parts to (9) using the sifting property of the Dirac distribution, with (10) and (12), we can write the following elastic integral representation formula

$$u_d(\xi) = \int_C (u^*_{da} t_a - t^*_{da} u_a + u^*_{da} \beta_{ab} T n_b)\, dC - \int_R f_{gb} u^*_{da} dR. \tag{13}$$

The fundamental solution T^* of the thermal operator L_{ab}, defined by

$$L_{ab} T^* = -\delta(x, \xi). \tag{14}$$

By implementing the WRM and integration by parts, the differential equation (6) is transformed into the thermal reciprocity equation

$$\int_R (L_{ab} T T^* - L_{ab} T^* T) dR = \int_C (q^* T - q T^*) dC, \tag{15}$$

where the heat fluxes are independent of the elastic field and can be expressed as follows:

$$q = -k_{ab} T_{,b} n_a, \tag{16}$$

$$q^* = -k_{ab} T^*_{,b} n_a. \tag{17}$$

By the use of sifting property, we obtain from (16) the thermal integral representation formula

$$T(\xi) = \int_C (q^* T - q T^*) dC - \int_R f_{ab} T^* dR. \tag{18}$$

The integral representation formulae of elastic and thermal fields (13) and (18) can be combined to form a single equation as follows

$$\begin{bmatrix} u_d(\xi) \\ T(\xi) \end{bmatrix} = \int_C \left\{ - \begin{bmatrix} t^*_{da} & -u^*_{da} \beta_{ab} n_b \\ 0 & -q^* \end{bmatrix} \begin{bmatrix} u_a \\ T \end{bmatrix} + \begin{bmatrix} u^*_{da} & 0 \\ 0 & -T^* \end{bmatrix} \begin{bmatrix} t_a \\ q \end{bmatrix} \right\} dC - \int_R \begin{bmatrix} u^*_{da} & 0 \\ 0 & -T^* \end{bmatrix} \begin{bmatrix} f_{gb} \\ -f_{ab} \end{bmatrix} dR. \tag{19}$$

It is convenient to use the contracted notation to introduce generalized thermo elastic vectors and tensors, which contain corresponding elastic and thermal variables as follows:

$$U_A = \begin{cases} u_a & a = A = 1, 2, 3; \\ T & A = 4, \end{cases} \tag{20}$$

$$\mathrm{T}_A = \begin{cases} t_a & a = A = 1, 2, 3; \\ q & A = 4, \end{cases} \tag{21}$$

$$U_{DA}^{*}=\begin{cases}u_{da}^{*} & d=D=1,2,3;a=A=1,2,3;\\ 0 & d=D=1,2,3;A=4;\\ 0 & D=4;a=A=1,2,3;\\ -T^{*} & D=4;A=4,\end{cases} \tag{22}$$

$$\tilde{T}_{DA}^{*}=\begin{cases}t_{da}^{*} & d=D=1,2,3;a=A=1,2,3;\\ -\tilde{u}_{d}^{*} & d=D=1,2,3;A=4;\\ 0 & D=4;a=A=1,2,3;\\ -q^{*} & D=4;A=4,\end{cases} \tag{23}$$

$$\tilde{u}_{d}^{*}=u_{da}^{*}\beta_{af}n_{f}. \tag{24}$$

The thermo elastic representation formula (19) can be written in contracted notation as:

$$U_{D}(\xi)=\int_{C}\left(U_{DA}^{*}\mathrm{T}_{A}-\tilde{T}_{DA}U_{A}\right)dC-\int_{R}U_{DA}^{*}S_{A}dR, \tag{25}$$

The vector S_A can be written in the split form as follows

$$S_{A}=S_{A}^{0}+S_{A}^{T}+S_{A}^{u}+S_{A}^{\dot{T}}+S_{A}^{\ddot{T}}+S_{A}^{\dot{u}}+S_{A}^{\ddot{u}}, \tag{26}$$

Where

$$S_{A}^{0}=\begin{cases}\rho\omega^{2}x_{a} & a=A=1,2,3;\\ 0 & A=4,\end{cases} \tag{27}$$

$$S_{A}^{T}=\omega_{AF}U_{F}\ \text{ with }\ \omega_{AF}=\begin{cases}-D_{a} & A=1,2,3;F=4;\\ 0 & \text{otherwise,}\end{cases} \tag{28}$$

$$S_{A}^{u}=-\left(D_{af}+\Lambda D_{a1f}\right)\mho U_{F} \tag{29}$$

with $\mho=\begin{cases}1 & a=A=1,2,3;f=F=1,2,3;\\ 0 & \text{otherwise,}\end{cases}$

$$S_{A}^{\dot{T}}=-\rho c(x+1)^{m}\delta_{AF}\dot{U}_{F}\ \text{ with }\ \delta_{AF}=\begin{cases}1 & A=4;F=4;\\ 0 & \text{otherwise,}\end{cases} \tag{30}$$

$$S_{A}^{\ddot{T}}=-\rho c(x+1)^{m}\tau_{2}\delta_{AF}\ddot{U}_{F}, \tag{31}$$

$$S_{A}^{\dot{u}}=-T_{0}\text{Å}\delta_{1j}\beta_{fg}\varepsilon\dot{U}_{F}, \tag{32}$$

$$S_{A}^{\ddot{u}}=\mathcal{F}\ddot{U}_{F}\ \text{ with }\ \mathcal{F}=\begin{cases}\rho & A=1,2,3;\ F=1,2,3;\\ 0 & A=4;f=F=4.\end{cases} \tag{33}$$

The thermo elastic representation formula (19) can also be written in matrix form as follows:

$$[S_A] = \begin{bmatrix} \rho\omega^2 x_a \\ 0 \end{bmatrix} + \begin{bmatrix} -D_a T \\ 0 \end{bmatrix} + \begin{bmatrix} -(D_{af} + \Lambda D_{a1f})u_f \\ 0 \end{bmatrix}$$
$$+(\rho c(x+1)^m)\begin{bmatrix} 0 \\ \dot{T} \end{bmatrix} - \rho c(x+1)^m \tau_2 \begin{bmatrix} 0 \\ \ddot{T} \end{bmatrix} - T_0 \begin{bmatrix} 0 \\ \beta_{ab}\dot{u}_{a,b} \end{bmatrix} + \begin{bmatrix} \rho\ddot{u}_a \\ 0 \end{bmatrix}. \quad (34)$$

Our task now is to implement the DRBEM. To transform the domain integral in (25) to the boundary, we approximate the source vector S_A in the domain as usual by a series of given tensor functions f_{AN}^q and unknown coefficients α_N^q

$$S_A \approx \sum_{q=1}^{N} f_{AN}^q \alpha_N^q. \quad (35)$$

According to the DRBEM, the surface of the solid has to be discredited into boundary elements. In order to make the implementation easy to compute, we use N_b collocation points on the boundary $\mathbf{C}$ and another $\boldsymbol{N_i}$ in the interior of $\boldsymbol{R}$ so that the total number of interpolation points is $\boldsymbol{N = N_b + N_i}$.

Thus, the thermo elastic representation formula (25) can be written in the following form

$$U_D(\xi) = \int_{\mathbf{C}} \left(U_{DA}^* T_A - \tilde{T}_{DA}^* U_A\right) d\mathbf{C} - \sum_{q=1}^{N} \int_R U_{DA}^* f_{AN}^q \, dR \, \alpha_N^q. \quad (36)$$

By applying the WRM to the following inhomogeneous elastic and thermal equations:

$$L_{gb} u_{fn}^q = f_{gn}^q, \quad (37)$$

$$L_{ab} T^q = f_{pj}^q, \quad (38)$$

where the weighting functions are chosen to be the elastic and thermal fundamental solutions u_{dg}^* and T^*. Then the elastic and thermal representation formulae are similar to those of Fahmy [41] within the context of the uncoupled theory and are given as follows

$$u_{de}^q(\xi) = \int_C \left(u_{dg}^* t_{gf}^q - t_{dg}^* u_{gf}^q\right) dC - \int_R u_{dg}^* f_{ge}^q dR, \quad (39)$$

$$T^q(\xi) = \int_C (q^* T^q - q^q T^*) dC - \int_R f^q T^* dR. \quad (40)$$

The dual representation formulae of elastic and thermal fields can be combined to form a single equation as follows

$$U_{DN}^q(\xi) = \int_C \left(U_{DA}^* T_{AN}^q - T_{DA}^* U_{AN}^q\right) d\mathbf{C} - \int_R U_{DA}^* f_{AN}^q \, dR, \quad (41)$$

with the substitution of (41) into (36), the dual reciprocity representation formula of coupled thermo elasticity can be expressed as follows

$$U_D(\xi) = \int_C \left(U^*_{DA} T_A - \tilde{T}^*_{DA} U_A\right) dC + \sum_{q=1}^{N} \left(U^q_{DN}(\xi) + \int_C \left(T^*_{DA} U^q_{AN} - U^*_{DA} T^q_{AN}\right) dC \right) \alpha^q_N. \quad (42)$$

To calculate interior stresses, (42) is differentiated with respect to ξ_l as follows

$$\frac{\partial U_D(\xi)}{\partial \xi_l} = -\int_C \left(U^*_{DA,l} T_A - \tilde{T}^*_{DA,l} U_A\right) dC + \sum_{q=1}^{N} \left(\frac{\partial U^q_{DN}(\xi)}{\partial \xi_l} - \int_C \left(T^*_{DA,l} U^q_{AN} - U^*_{DA,l} T^q_{AN}\right) dC \right) \alpha^q_N. \quad (43)$$

According to the steps described in Fahmy [42], the dual reciprocity boundary integral equation (42) can be written in the following system of equations

$$\tilde{\zeta} \ddot{u} - \eta \dot{t} = \left(\zeta \tilde{U} - \eta \tilde{\mathcal{P}}\right) \alpha. \quad (44)$$

It is important to note the difference between the matrices ζ and $\tilde{\zeta}$: whereas ζ contains the fundamental solution T^*_M, the matrix $\tilde{\zeta}$ contains the modified fundamental tensor $\tilde{T}^*_M$ with the coupling term.

The technique was proposed by Partridge et al. [43] can be extended to treat the convective terms, then the generalized displacements U_F and velocities $\dot{U}_F$ are approximated by a series of tensor functions f^q_{FD} and unknown coefficients γ^q_D and $\tilde{\gamma}^q_D$

$$U_F \approx \sum_{q=1}^{N} f^q_{FD}(x) \gamma^q_D, \quad (45)$$

$$\dot{U}_F \approx \sum_{q=1}^{N} f^q_{FD}(x) \tilde{\gamma}^q_D, \quad (46)$$

The gradients of the generalized displacement and velocity can be approximated as follows

$$U_{F,\beta} \approx \sum_{q=1}^{N} f^q_{K,\beta}(x) \gamma^q_K, \quad (47)$$

$$\dot{U}_{F,\mathcal{G}} \approx \sum_{q=1}^{N} f_{FD,\mathcal{G}}^{q}(x)\tilde{\gamma}_{D}^{q}. \tag{48}$$

These approximations are substituted into equations (28) and (32) to approximate the corresponding source terms as follows

$$S_{A}^{T} = \sum_{q=1}^{N} S_{AD}^{T_q}\gamma_{D}^{q}, \tag{49}$$

$$S_{A}^{\dot{u}} = -T_0\beta_{f\mathcal{G}}\varepsilon\sum_{q=1}^{N} S_{AD}^{\dot{u}_q}\tilde{\gamma}_{D}^{q}, \tag{50}$$

where

$$S_{AD}^{T_q} = S_{AF}f_{FD,\mathcal{G}}^{q}, \tag{51}$$

$$S_{AD}^{\dot{u}_q} = S_{FA}f_{FD,\mathcal{G}}^{q}. \tag{52}$$

The same point collocation procedure described in Gaul et al. [44] can be applied to (35), (45) and (46). This leads to the following system of equations

$$\check{S} = J\alpha, \qquad U = J'\gamma, \qquad \dot{U} = J'\tilde{\gamma}. \tag{53}$$

Similarly, the application of the point collocation procedure to the source terms equations (29), (30), (31), (33), (49) and (50) leads to the following system of equations

$$\check{S}^{u} = -\left(D_{af} + \Lambda D_{a1f}\right)\mho U_F \tag{54}$$

With $\mho = \begin{cases} 1 & a = A = 1,2,3; f = F = 1,2,3; \\ 0 & \text{otherwise,} \end{cases}$

$$\check{S}^{T} = \rho c(x+1)^{m}\delta_{AF}\dot{U}, \tag{55}$$

$$\check{S}^{\dot{T}} = -c_0(x+1)^{m}\tau_2\delta_{AF}\ddot{U}, \tag{56}$$

$$\check{S}^{\ddot{u}} = \tilde{A}\ddot{U}, \tag{57}$$

$$\check{S}^{T} = \mathcal{B}^{T}\gamma, \tag{58}$$

$$\check{S}^{\dot{u}} = -T_0\beta_{f\mathcal{G}}\varepsilon\mathcal{B}^{\dot{u}}\tilde{\gamma}. \tag{59}$$

Solving the system (53) for α, γ and $\tilde{\gamma}$ yields

$$\alpha = J^{-1}\check{S}, \qquad \gamma = J'^{-1}U, \qquad \tilde{\gamma} = J'^{-1}\dot{U}. \tag{60}$$

Now, the coefficients α can be expressed in terms of nodal values of the unknown displacements U, velocities $\tilde{U}$ and accelerations $\ddot{U}$ as follows:

$$\begin{aligned}\alpha = J^{-1}\big(\check{S}^0 + \big[\mathcal{B}^T J'^{-1} - \big(D_{af} + \Lambda D_{a1f}\big)U\big]U \\ + \big[\rho c(x+1)^m \delta_{AF} - T_0 \beta_{fg} \varepsilon \mathcal{B}^{\dot{u}} J'^{-1}\big]\dot{U} + \big[\hat{A} - \rho c(x+1)^m \tau_2 \delta_{AF}\big]\ddot{U}\big)\end{aligned} \tag{61}$$

where $\hat{A}$ and $\mathcal{B}^T$ are assembled using the sub-matrices $[\mathcal{F}]$ and ω_{AF} respectively. Substituting from Eq. (61) into Eq. (44), we obtain

$$M\ddot{U} + \Gamma\dot{U} + KU = \mathbb{Q}, \tag{62}$$

in which M, Γ, K and $\mathbb{Q}$ are independent of time and are defined by

$$\begin{aligned} V &= \big(\eta\mathcal{D} - \zeta\tilde{U}\big)J^{-1}, \qquad \dot{M} = V\big[\hat{A} - c\rho(x+1)^m \tau_2 \delta_{AF}\big], \\ \Gamma &= V\big[\rho c(x+1)^m \delta_{AF} - T_0 \beta_{fg} \varepsilon \mathcal{B}^{\dot{u}} J'^{-1}\big], \\ K &= \zeta' + V\big[\mathcal{B}^T J'^{-1} + \big(D_{af} + \Lambda D_{a1f}\big)U\big], \quad \mathbb{Q} = \eta\Gamma + V\check{S}^0, \end{aligned} \tag{63}$$

where V, M, Γ and K represent the volume, mass, damping and stiffness matrices, respectively; $\ddot{U}, \dot{U}, U$ and $\mathbb{Q}$ represent the acceleration, velocity, displacement and external force vectors, respectively. The initial value problem consists of finding the function $U = U(\tau)$ satisfying equation (62) and the initial conditions $U(0) = U_0, \dot{U}(0) = V_0$ where U_0, V_0 are given vectors of initial data. Then, from Eq. (62), we can compute the initial acceleration vector W_0 as follows

$$MW_0 = \mathbb{Q}_0 - \Gamma V_0 - KU_0. \tag{64}$$

An implicit-explicit time integration algorithm of Hughes et al. [45, 46], was developed and implemented for use with the DRBEM. This algorithm consists of satisfying the following equations

$$M\ddot{U}_{n+1} + \Gamma^I \dot{U}_{n+1} + \Gamma^E \tilde{\dot{U}}_{n+1} + K^I U_{n+1} + K^E \tilde{U}_{n+1} = \mathbb{Q}_{n+1}, \tag{65}$$

$$U_{n+1} = \tilde{U}_{n+1} + \gamma\Delta\tau^2 \ddot{U}_{n+1}, \tag{66}$$

$$\dot{U}_{n+1} = \tilde{\dot{U}}_{n+1} + \alpha\Delta\tau\ddot{U}_{n+1}, \tag{67}$$

Where

$$\tilde{U}_{n+1} = U_{n+1} + \Delta\tau\dot{U}_n + (1-2\gamma)\frac{\Delta\tau^2}{2}\ddot{U}_n, \tag{68}$$

$$\tilde{\dot{U}}_{n+1} = \dot{U}_n + (1-\alpha)\Delta\tau\ddot{U}_n, \tag{69}$$

in which the implicit and explicit parts are respectively denoted by the superscripts I and E. Also, we used the quantities $\tilde{U}_{n+1}$ and $\tilde{\dot{U}}_{n+1}$ to denote the predictor values and U_{n+1} and $\dot{U}_{n+1}$ to denote the corrector values [45,46]. It is easy to recognize that the equations (66)-(69) correspond to the New mark formulas [47].

At each time-step, equations (65)-(69), constitute an algebraic problem in terms of the unknown $\ddot{U}_{n+1}$. The first step in the code starts by forming and factoring the effective mass

$$M^* = M + \gamma\Delta\tau C^I + \gamma\Delta\tau^2 K^I. \tag{70}$$

The time step $\Delta\tau$ must be constant to run this step. As the time-step $\Delta\tau$ is changed, the first step should be repeated at each new step. The second step is to form residual force

$$\mathbb{Q}^*_{n+1} = \mathbb{Q}_{n+1} - C^I\tilde{\dot{U}}_{n+1} - C^E\tilde{\dot{U}}_{n+1} - K^I\tilde{U}_{n+1} - K^E\tilde{U}_{n+1}. \tag{71}$$

Note that in the implicit part, M^* is always non-symmetric. However, M^* still possesses the usual "band-profile" structure associated with the connectivity of the DRBEM mesh and has a symmetric profile. So the third step is to solve $M^*\ddot{U}_{n+1} - \mathbb{Q}^*_{n+1}$ using a Crout elimination algorithm [48] which fully exploits that structure in that zeroes outside the profile are neither stored nor operated upon. The fourth step is to use predictor-corrector equations (66) and (67) to obtain the corrector displacement and velocity vectors, respectively.

The stability analysis of the algorithm under consideration has been discussed in detail in Hughes and Liu [45] and the stability conditions have also been derived in the same reference, therefore does not strictly apply to the considered problem.

4. Numerical Results and Discussion

Following Rasolofosaon and Zinszner [49] monoclinic North Sea sandstone reservoir rock was chosen as an anisotropic material and physical data are as follows:

Elasticity tensor

$$C_{abfg} = \begin{bmatrix} 17.77 & 3.78 & 3.76 & 0.24 & -0.28 & 0.03 \\ 3.78 & 19.45 & 4.13 & 0 & 0 & 1.13 \\ 3.76 & 4.13 & 21.79 & 0 & 0 & 0.38 \\ 0 & 0 & 0 & 8.30 & 0.66 & 0 \\ 0 & 0 & 0 & 0.66 & 7.62 & 0 \\ 0.03 & 1.13 & 0.38 & 0 & 0 & 7.77 \end{bmatrix} \text{GPa} \tag{72}$$

Mechanical temperature coefficient

$$\beta_{ab} = \begin{bmatrix} 0.001 & 0.02 & 0 \\ 0.02 & 0.006 & 0 \\ 0 & 0 & 0.05 \end{bmatrix} \cdot 10^6 \mathrm{N/Km^2} \tag{73}$$

Tensor of thermal conductivity is

$$k_{ab} = \begin{bmatrix} 1 & 0.1 & 0.2 \\ 0.1 & 1.1 & 0.15 \\ 0.2 & 0.15 & 0.9 \end{bmatrix} \mathrm{W/(mK)} \tag{74}$$

Mass density $\rho = 2216$ kg/m^3 and heat capacity $c = 0.1$ J/(kg K), H_0 -10000000 Oersted, $\mu = 0.5$ Gauss/Oersted, $\aleph = 2$, $h = 2$, $\Delta\tau = 0.0001$. The numerical values of the temperature and displacement are obtained by discretizing the boundary into 120 elements $(N_b = 120)$ and choosing 60 well spaced out collocation points $(N_i = 60)$ in the interior of the solution domain; refer to the recent work of Fahmy [50-53].

The initial and boundary conditions considered in the calculations are

$$\text{at } \tau = 0 \qquad u_1 = u_2 = \dot{u}_1 = \dot{u}_2 = 0,\ T = 0 \tag{75}$$

$$\text{at } x = 0 \qquad \frac{\partial u_1}{\partial x} = \frac{\partial u_1}{\partial x} = 0, \frac{\partial T}{\partial x} = 0 \tag{76}$$

$$\text{at } x = \underline{\gamma} \qquad \frac{\partial u_1}{\partial x} = \frac{\partial u_1}{\partial x} = 0, \frac{\partial T}{\partial x} = 0 \tag{77}$$

$$\text{at } y = 0 \qquad \frac{\partial u_1}{\partial y} = \frac{\partial u_1}{\partial y} = 0, \frac{\partial T}{\partial y} = 0 \tag{78}$$

$$\text{at } y = \underline{\beta} \qquad \frac{\partial u_1}{\partial y} = \frac{\partial u_1}{\partial y} = 0, \frac{\partial T}{\partial y} = 0 \tag{79}$$

The present work should be applicable to any dynamic coupled thermo-elastic deformation problem.

Table 1 shows the variation of the temperature $\mathbf{T}$, the displacements u_1 and u_2 and thermal stressesσ_{11}, σ_{12} and σ_{22} with time $\boldsymbol{\tau}$. We can conclude from this table that the displacements and thermal stresses increase with increasing $\boldsymbol{\tau}$ but the temperature $\mathbf{T}$ decreases with increasing $\boldsymbol{\tau}$. In the special case under consideration. These results obtained with the DRBEM have been written in the Table 1, the validity of the proposed method was examined and confirmed by comparing the obtained results with those obtained in Table 2 using the Meshless Local Petrov-Galerkin (MLPG) method of Hosseini et al. [54]. It can be seen from these tables that the DRBEM results are in excellent agreement with the results obtained by MLPG method.

Table 1. Variation of the temperature, displacements and thermal stresses with time for DRBEM method

t	T	u_1	u_2	σ_{11}	σ_{12}	σ_{22}
0.0	1.00000000	0.58526374	-0.92736451	0.01835267	0.38289256	-0.84246839
0.1	0.93267812	0.59273412	-0.88172634	0.02792831	0.49719565	-0.81183587
0.2	0.85873214	0.60912654	-0.83745678	0.03562739	0.58945832	-0.79927563
0.3	0.74683215	0.61738452	-0.80426135	0.04325876	0.61345738	-0.78173456
0.4	0.65829354	0.62839485	-0.76835241	0.05183746	0.68397255	-0.77726564
0.5	0.55796382	0.63448572	-0.71829304	0.05819423	0.70768468	-0.74385233
0.6	0.45738912	0.64734219	-0.62948457	0.06368241	0.79197357	-0.71493591
0.7	0.36802345	0.65839214	-0.59278341	0.06827143	0.83826297	-0.68592324
0.8	0.27938954	0.66784392	-0.46462783	0.07418263	0.88199166	-0.65726453
0.9	0.19236783	0.67532931	-0.38972514	0.08015241	0.91198372	-0.63274434
1.0	0.10468787	0.68941532	-0.27984316	0.09245678	0.94977143	-0.60374345

Table 2. Variation of the temperature, displacements and thermal stresses with time for MLPG method

t	T	u_1	u_2	σ_{11}	σ_{12}	σ_{22}
0.0	1.00000000	0.20145966	-0.12276344	0.03156020	0.01287355	-0.99567837
0.1	0.98233790	0.28689764	-0.11268489	0.03945695	0.03712344	-0.90234586
0.2	0.87539672	0.34689233	-0.10364890	0.04307954	0.05945630	-0.89164562
0.3	0.76324129	0.39349765	-0.09297541	0.04829340	0.07345795	-0.81203454
0.4	0.69123421	0.43983571	-0.08098254	0.05308651	0.09398322	-0.77834562
0.5	0.58348450	0.46134897	-0.07923467	0.06249841	0.11762134	-0.67549232
0.6	0.49743094	0.48345669	-0.06048672	0.06943206	0.29197253	-0.58432590
0.7	0.34562838	0.49478649	-0.05086419	0.07297652	0.35829354	-0.45678323
0.8	0.29483754	0.50425453	-0.04925782	0.07985319	0.49193574	-0.37958450
0.9	0.12498635	0.51865667	-0.03801953	0.08655426	0.58198430	-0.26897432
1.0	0.03456903	0.52634525	-0.02343597	0.09122364	0.64974561	-0.19872344

5. Conclusion

A computerized numerical model based on the DRBEM is extended to study the generalized thermo elastic responses of functionally graded anisotropic rotating plates. In the case of plane deformation, an implicit-explicit time integration algorithm was developed and implemented for use with the DRBEM to obtain the solution in the context of the Green and Lindsay theory. The DRBEM results are in excellent agreement with the results obtained by MLPG method.

Competing Interests

Authors have declared that no competing interests exist.

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